## Cascade control

## In class activities

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## Activities

1. Effect of delay time on controller tuning

Consider a process with following transfer function

$$G_p = \frac{1}{(5s+1)(3s+1)} \tag{1}$$

The PI controller for this process has parameters of  $K_c = 3$ , and  $\tau_1 = 6$ .

What happens to the response when a dead time of  $\theta$  = 2 is introduced?

Determine controller parameters to obtain an overshoot similar to the process without delay.

- 2. Design a Smith predictor for problem 1.
- 3. It is desired to control the size distribution of crystals produced in vacuum continuous crystallizer, but it's very difficult to measure i.e. requires lengthy lab test. Some experiment suggest that crystal size distribution are strongly related to the (1) stirrer speed q, (2) magma temperature T, (3) degree of supersaturation C-Cs, and (4) mother liquor density r. C is concentration of the solute and Cs is the solubility of the solute.
  - 1. Suggest an inferential control technique for crystal size distribution
  - 2. Show the schematic of the control strategy. Comment on the effectiveness of the strategy.
- 4. Consider two inferential model for the prediction of distillation top impurity fraction xD and a tray temperature T as follows: Reduction in the heavy key fraction in the feed by 10%:

$$T = 60 + 9.5x_D; 0 \le x_D \le 0.1 \tag{2}$$

Increase in the heavy key fraction in the feed by 10%:

$$T = 60.1 + 11.8x_D; 0 \le x_D \le 0.1 \tag{3}$$

To ensure that the impurity in the distillate remains within 5%, what would be the setpoint to the inferential tray temperature controller? Explain how you would determine the appropriate setpoint value.

5. **Gain Scheduling**: For the furnace shown in Figure 1, show a schematic control strategy with gain scheduling. What variable can you use for gain scheduling? Give your reasons.



Figure 1: Furnace

6. A cold process fluid is heated up in a shell-and-tube heat exchanger using steam. At the nominal process feed flow rate, the transfer function of the exit temperature of the process fluid is given as follows:

$$G_p = \frac{exp(-2s)}{(5s+1)} \tag{4}$$

It has been found that the process gain is strongly related to the process fluid flow rate given as follows:

$$K_p = 1 + 0.5\Delta F_p \tag{5}$$

Where,  $\Delta F_p$  denotes the change of process fluid flow rate from its nominal value, i.e.,  $\Delta F_p = F_p - \bar{F}_p$  where  $F_p$  is the current value of process fluid flow rate and  $\bar{F}_p$  the nominal value (steady-state) of the process fluid flow rate.

An ideal PI controller is given by

$$G_c = K_c \left( 1 + \frac{1}{\tau_I s} \right) \tag{6}$$

Based on the PI controller tuning via the stability-based formula,

$$K_c = \left(\frac{r_p}{K_p}\right) \left(\frac{\tau_p}{\theta_p}\right); 0 < r_p < 1 \tag{7}$$

and

$$\tau_I = \tau_p \tag{8}$$

Assume the baseline or nominal value of the process fluid flow rate is  $\bar{F}_p=2$ , calculate the values in Table 1.

F <sub>p</sub>	K <sub>p</sub>	K <sub>c</sub>
2 (nominal)	1	1.75
3	1.5	1.17
1	0.5	3.5

Table 1: Tuning parameters	for	problem 5
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Note: To calculate  $K_c$  a value of  $r_p$  = 0.7 was used.

Evaluate the controller performance. Simulink file for problem implementation without gain scheduling is given here.

## 7. Reactor-Furnace-Distillation System:

For RFD system shown in Figure 2, draw the schematic of LS control strategy for the reactor system, where it is desired to control the component A (CA), and temperature of the reactor effluent T. The reactor temperature should not exceed Tmax due to the possibility of the process encountering runaway reaction and instability.



Figure 2: Reactor-Furnace-Distillation system